
Note

The role of constitutive equations in chemical kinetics

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Recent articles on the non-isothermal rate equation^{1–3} have initiated a rather extensive discussion^{4–13}. Misunderstanding arose mainly about the meaning of the partial derivatives of the function f in the equation for the fractional conversion α , (a kinetic variable conventionally normalized $\alpha = 0$ at $t = 0$ and $\alpha = 1$ at $t \rightarrow \infty$):

$$\alpha = f(T, t) \quad (1)$$

$$d\alpha = \left(\frac{\partial f}{\partial T} \right)_t dt + \left(\frac{\partial f}{\partial t} \right)_T dT \quad (2)$$

where T and t represent temperature and time, respectively. Some authors claimed that only the partial derivative $(\partial f / \partial t)_T$ can be used so that the function f is appropriate for the description of an isothermally measured rate of a chemical reaction^{1–3}, while others proposed that it may describe non-isothermal kinetics as well if either the partial derivative $(\partial f / \partial T)_t$ ⁴ or the total differential $d\alpha$ ⁵ are equal to zero. Another suggestion⁶ related this problem to the non-uniform temperature within a solid sample. Although some useful criticism on these incorrect ideas was already given^{7–13} and the path function character of f in eqn (1) emphasized^{8,9} there still remain certain confusions. Therefore we would like to clarify this question from a more unifying viewpoint.

We will mention two different ways in which the relation (1) may be understood:

(A) If eqn (1) represents an equation of state (called “the constitutive equation”) of a chemical system under consideration then eqn (1) implies that the value α at t depends on the time t , and the instantaneous value of the temperature T at t regardless of its previous temperature history. The constitutive equation of type (1) would describe the behaviour of a system controlled by an independent “internal clock”. Such an equation is *e.g.* the constitutive equation for the pressure p of a gas which is evolved by a radioactive decay. The number of molecules produced is controlled by the radioactive mechanism and is not affected by the temperature. The pressure p is expressed by a function P of the number of molecules, i.e. a function of time t , and the temperature T at t only, $p = P(T, t)$.

It seems that ordinary chemical systems treated so far by the standard methods of chemical kinetics^{1,4} do not represent the case of systems with an "internal clock". The controversy concerning the total differential dx and the partial derivatives $(\partial f/\partial T)_t$ and/or $(\partial f/\partial t)_T$ which appears in some preceding papers¹⁻⁵ is a consequence of the application of the described non-adequate interpretation of eqn (1) for ordinary chemical systems.

(B) We are convinced that the constitutive equation for the fractional conversion x determined in a chemical system is

$$\dot{x} = F(x, T) \quad (3)$$

or in a more general form

$$\dot{x} = G(x, T, \dot{T}, \ddot{T}, \dots) \quad (4)$$

Equations of the eqn (3) type are well established in isothermal kinetics^{7,11,14}. Equation (4) which has the form known for non-equilibrium situations could be more appropriate in the case of highly non-isothermal kinetics.

Based on eqn (3) or (4) eqn (1) may be interpreted as follows. For the initial conditions ($x = 0$ and $T = T_0$ at $t = 0$) and a specified temperature regime. $T = \Phi(t)$, we denote the solution of eqn (3) or (4) as

$$x = x_\Phi(t). \quad (5)$$

Note that the subscript Φ indicates that the solution depends on the temperature regime $\Phi(t)$, i.e. x is path dependent. In mathematical terms it means that x is a functional of Φ .

For some special instances of "temperature" kinetics solution (5) can be converted into the form (1). We illustrate this for a simple case of the "linear" non-isothermal kinetics, where

$$T = \Phi(t) = \phi t + T_0 \quad (6)$$

and where ϕ is the constant temperature rate. When substituting eqn (6) into eqn (3) we obtain $\dot{x} = F(x, \phi t + T_0)$ or similarly from eqn (4) $\dot{x} = G(x, \phi t + T_0, \phi, 0, \dots)$. The solution (5) can then be written in the form $x = g_0(\phi, T_0, t)$. It means that the functional dependence (5) is reduced to the function dependence of x on two parameters ϕ and T_0 which specify the temperature regime Φ . If we compare the evolution of the fractional conversion x for multiple runs accomplished at different ϕ holding the initial temperature T_0 fixed, we can write

$$x = g_0(\phi, T_0, t) \equiv g(\phi, t) = g((T - T_0)/t, t) \equiv f_0(T, T_0, t) = f(T, t) \quad (7)$$

If we understand eqn (1) in the described sense, which is illustrated by eqn (7), then the interpretation of the total differential dx and the partial derivatives, namely $(\partial f/\partial T)_t$, represents no principal difficulty. For a specified class of temperature regimes eqn (6) the eqn (7) can be properly represented as a surface in a three-dimensional diagram $x-t-\phi$. Then it is easy to realize that within this specified class of

temperature regimes ϕ the isochronal derivative $(\partial g/\partial \phi)_t$, indicates the change of x measured at the same time t between two infinitesimally close regimes differing by $d\phi$, i.e. between two parallel $x-t$ curves which are the sections of the surface taken at ϕ and $\phi + d\phi$. Similarly we can interpret the derivative $(\partial f/\partial T)_t$ using the $x-t-T$ diagram. A more comprehensive discussion of the meaning of the partial derivatives was dealt with in our previous paper¹³.

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